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PATENT

**RUBIDIUM TITANYL ARSENATE-SILVER GALLIUM SELENIDE
TANDEM OPTICAL PARAMETRIC OSCILLATOR**

J. M. Fukumoto

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CROSS-REFERENCE TO RELATED APPLICATIONS

10 This application is a continuation-in-part of U.S. Patent Application no.
09/478,229, entitled MONOLITHIC SERIAL OPTICAL PARAMETRIC
OSCILLATOR filed January 06, 2000, by J. M. Fukumoto (Atty. Docket No. PD
99W073). In addition, this application relates to copending application no.
_____ entitled EFFICIENT ANGLE TUNABLE OUTPUT FROM A
15 MONOLITHIC SERIAL KTA OPTICAL PARAMETRIC OSCILLATOR, filed
_____ by J. M. Fukumoto (Atty. Docket No. PD 01W0007).

BACKGROUND OF THE INVENTION

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Field of the Invention:

25 The present invention relates to solid state lasers and frequency shifting of
laser output. More specifically, the present invention relates to frequency shifted solid
state laser output operative in the 8 – 12 micron range.

Description of the Related Art:

Lasers are currently widely used for communication, research and development, manufacturing, directed energy and numerous other applications. For many applications, the energy efficiency, power and light weight of solid state lasers make these devices particularly useful. Because only a few crystals lase and each crystal lases at a unique fundamental frequency, the wavelengths which can be generated by a laser are limited.

Solid state lasers currently lase in the range of one to three microns. For certain applications, there is a need to reach longer laser operating wavelengths. In particular, there is interest in the 8 - 12 micron (μm) region. A system which can generate pulsed, tunable radiation at these wavelengths is particularly useful for the remote detection of chemical agents and other chemical species. Unfortunately, the 8-12 μm region is a very difficult wavelength region to access. No current solid-state laser source is capable of emitting pulsed, tunable laser output in this region.

Wavelength conversion of commonly available 1 micron lasers to the 8-12 micron region using optical parametric oscillators (OPOs) and difference frequency generation (DFG) has been demonstrated, but the overall energy conversion efficiencies were low. See for example: 1) S. Chandra, T. H. Allik, G. Catella, R. Utano, J. A. Hutchinson, "Continuously tunable 6-14 μm silver gallium selenide optical parametric oscillator pumped at 1.57 μm ," Appl. Phys. Lett. **71**, 584-586 (1997); and 2) R. Utano and M. J. Ferry, "8-12 μm generation using difference frequency generation in AgGaSe_2 of a Nd:YAG pumped KTP OPO," in *Advanced Solid State Lasers, OSA Trends in Optics and Photonics* (Optical Society of America, Washington, D. C., 1997), Vol. 10, pp. 267-269.

One approach involved the use of a 1 micron laser to pump a potassium titanyl phosphate (KTP) OPO, whose signal wave output at 1.57 microns was then used to pump a silver gallium selenide (AgGaSe_2) OPO to produce 6-14 micron output. Optical parametric oscillators (OPOs) have been widely used to shift the fundamental

output of a laser from one wavelength to another through the use of a nonlinear crystal. Unfortunately, the use of OPOs limits the efficiency of the system. This is due to the fact that the energy in the input laser beam is split between plural output beams. In the described system, the KTP OPO output is a less than optimal pump
5 source for the AgGaSe₂ OPO.

Hence, a need remains in the art for an efficient, tunable system or method for converting the output of a typical 1 μm laser to the 8 - 12 μm range.

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SUMMARY OF THE INVENTION

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The need in the art is addressed by the present invention, a novel system and method for efficiently generating tunable pulsed laser output at 8-12 microns by converting the output of a standard 1 micron laser using a serial optical parametric oscillator (OPO) conversion scheme which uses the non-linear crystals rubidium titanyl arsenate (RTA) and silver gallium selenide (AgGaSe₂). This system can generate tunable 8-12 micron output in a more efficient manner than that which has been previously demonstrated. A key aspect of this approach is the use of the RTA
20 OPO to produce a secondary signal output at 3.01 microns with greater than 25% overall 1 micron to 3.01 micron conversion efficiency.

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The system includes a laser, a first optical parametric oscillator of unique design, and a second optical parametric oscillator. The first oscillator is constructed with an energy shifting crystal and first and second reflective elements disposed on either side thereof. Energy from the laser at a first wavelength is shifted by the crystal and output at a second wavelength. The second wavelength results from a secondary process induced by a primary emission of energy at a third wavelength, the third wavelength resulting from a primary process generated from the first wavelength in the crystal. Mirror coatings are applied on the reflective elements for containing the

primary emission and enhancing the secondary process. The second optical parametric oscillator then shifts the energy output by the first OPO at the second wavelength to the desired fourth wavelength. In the illustrative embodiment, the first optical parametric oscillator includes an x-cut rubidium titanyl arsenate crystal and the second optical parametric oscillator includes a silver gallium selenide crystal. The first wavelength is approximately 1.06 microns, the second wavelength is approximately 3.01 microns, the third wavelength is approximately 1.61 microns, and the fourth wavelength is in the range of 8-12 microns.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a diagram depicting a laser-based system for generating 8-12 micron wavelengths in accordance with the teachings of the present invention.

Fig. 2 is an illustration showing the wavelengths generated by the first stage OPO depicted in Fig. 1.

Fig. 3 is an illustration showing the secondary process caused by the primary process in the first stage OPO.

Fig. 4 is an illustration showing containment of the first process signal wave.

Fig. 5 is a diagram showing an RTA OPO for efficient generation of 3.01 μm output designed in accordance with teachings of the present invention.

DESCRIPTION OF THE INVENTION

5 Illustrative embodiments and exemplary applications will now be described with reference to the accompanying drawings to disclose the advantageous teachings of the present invention.

While the present invention is described herein with reference to illustrative
embodiments for particular applications, it should be understood that the invention is
10 not limited thereto. Those having ordinary skill in the art and access to the teachings provided herein will recognize additional modifications, applications, and embodiments within the scope thereof and additional fields in which the present invention would be of significant utility.

The present invention provides a novel system and method for generating
15 tunable pulsed laser output at 8-12 microns by converting the output of a standard 1 micron laser using a serial optical parametric oscillator (OPO) conversion scheme which uses the non-linear crystals rubidium titanyl arsenate (RTA) and silver gallium selenide (AgGaSe₂). This system can generate tunable 8-12 micron output in a more efficient manner than that which has been previously demonstrated.

20 Fig. 1 is a diagram depicting a laser-based system for generating 8-12 micron wavelengths in accordance with the teachings of the present invention. The system 10 is comprised of two stages. In the first stage, a 1 micron laser 12, such as a diode pumped Neodymium-Ytterbium Aluminum Garnet (Nd:YAG) laser, outputs a collimated beam of electromagnetic energy at a fundamental frequency of 1.06 μm .
25 This 1.06 μm beam is applied to an RTA OPO 14 consisting of an x-cut RTA crystal 20 sandwiched between a rear high reflector 16 and an output coupler 18. In the second stage, the 3.01 μm beam output from the RTA OPO 14 is applied to an AgGaSe₂ OPO 22 consisting of a Type II phase matched AgGaSe₂ crystal 24

sandwiched between a rear high reflector 26 and an output coupler 28, producing 8-12 μm output.

A 3.01 μm narrow band pass filter (not shown) can be placed between the first and second stages to prevent the 3.15 μm and 3.45 μm waves from pumping the
5 second stage.

A key aspect of this approach is the use of the RTA OPO 14 to produce a secondary signal output at 3.01 microns with greater than 25% overall 1 micron to 3.01 micron conversion efficiency. Direct lasing output at 3 microns has proven to be inefficient. Using a well-designed 1 micron diode-pumped solid-state laser and an
10 RTA OPO optimized to produce a secondary signal wave, an efficient 3.01 micron laser source will result.

The first stage conversion strategy has been described in detail for potassium titanyl arsenate (KTA) in the above-identified parent application (U.S. Patent Application no. 09/478,229, entitled MONOLITHIC SERIAL OPTICAL
15 PARAMETRIC OSCILLATOR filed January 06, 2000, by J. M. Fukumoto (Atty. Docket No. PD 99W073). A similar approach can be used with RTA to design an OPO optimized to produce a secondary signal wave at 3.01 μm .

Fig. 2 is an illustration showing the wavelengths generated by the RTA OPO 14 depicted in Fig. 1.

20 As is known in the art, in response to the application of a 1.06 μm pump beam thereto, the RTA crystal 20 generates a 1.61 μm signal wave and 3.15 μm idler wave. This is known as the 'primary process'.

However, not generally known in the art is the fact that as a result of this primary process, which is a serial process, a 'secondary process' occurs and is due to
25 the feedback of the 1.61 μm wave into the crystal by the reflectors 16 and 18 at the x-cut angle, an angle along one of the primary axes of the crystal. The secondary OPO process produces distinct signal and idler waves that are of longer wavelengths than those of the first OPO process. This is due to the fact that even a small amount of reflectivity (i.e., <10%) from either the crystal anti-reflection coatings or the OPO

mirrors at the secondary OPO signal wavelength can initiate oscillations at the secondary signal wavelength due to high gain and large acceptance angles of the secondary process. The crystal responds by generating the secondary signal and idler waves.

5 In the RTA crystal, the secondary process transforms some fraction of the 1.61 μm signal wave of the primary OPO process into secondary signal and idler waves at 3.01 μm and 3.45 μm , respectively. This is shown in the simplified diagram of Fig. 3, which depicts the newly discovered secondary process caused by the primary process in the first stage RTA OPO 14. In Fig. 3, the laser 12 and the reflective elements 16
10 and 18 have been omitted for clarity.

In Fig. 3, note that only a single crystal 20 is used, not two separate crystals. Nonetheless, those skilled in the art will appreciate that the present teachings may be extended to any number of mediums or crystals arranged in serial (cascade) or parallel configurations or any combination thereof without departing from the scope of the
15 present teachings.

Robust, tunable output at the wavelengths of the secondary process can be generated by maximizing the secondary OPO process (at the expense of the signal wave of the first process) through conscientious design of OPO mirror coatings. This is described more fully in the above-identified co-pending application entitled
20 EFFICIENT ANGLE TUNABLE OUTPUT FROM A MONOLITHIC SERIAL KTA OPTICAL PARAMETRIC OSCILLATOR, filed _____ by J. M. Fukumoto (Atty. Docket No. PD 01W0007) the teachings of which are hereby incorporated herein by reference.

Fig. 4 is an illustration showing containment of the first process signal wave.
25 The first process signal wave can be fully contained by the RTA OPO 14 by specifying high reflectivity at the first signal wavelength 1.61 μm and minimal reflectivity at the primary and secondary idler waves at 3.15 μm and 3.45 μm for both the rear reflector 16 and output coupler 18. The rear high reflector 16 should be highly reflective at 3.01 μm and highly transmissive at the pump wavelength of 1.06

μm . The output coupler 18 needs partial reflectivity at $3.01 \mu\text{m}$ in order to resonate the secondary signal wave for efficient $1 \mu\text{m}$ to $3.01 \mu\text{m}$ conversion. In this manner, the $1.61 \mu\text{m}$ pump wave for the secondary process is fully contained while the $3.01 \mu\text{m}$ signal wave for the secondary process is allowed to oscillate.

5 Fig. 5 is a diagram showing a preferred embodiment of the RTA OPO 14 for efficient generation of $3.01 \mu\text{m}$ output designed in accordance with teachings of the present invention. The OPO 14 includes a Type II x-cut ($\theta = 90^\circ$, $\phi = 0^\circ$) RTA crystal 20 sandwiched between a rear high reflector 16 and an output coupler 18. The reflective elements 16 and 18 are coated to contain or emit energy at desired
10 wavelengths. Those skilled in the art will be able to design reflective elements using optical thin films or other techniques known in the art and the invention is not limited to the design thereof. The rear reflector 16 has a first side 30 which receives the $1 \mu\text{m}$ pump beam, and a second side 32 which faces the crystal 20. The output coupler 18 a first side 34 which faces the crystal 20, and a second side 36 which faces the direction
15 of the output beam.

 In order to optimize the secondary process for the $3.01 \mu\text{m}$ secondary signal wave, the following coating specifications should be used:

- 20 - **Rear high reflector 16, first side 30:** anti-reflective (greater than 99% transmissive) coating at $1.064 \mu\text{m}$, 0° incidence; greater than 90% transmission at $3.15 \mu\text{m}$, 0° incidence; greater than 90% transmission at $3.45 \mu\text{m}$, 0° incidence.
- 25 - **Rear high reflector 16, second side 32:** greater than 97% transmission at $1.064 \mu\text{m}$, 0° incidence; greater than 99% reflection at $1.61 \mu\text{m}$, 0° incidence; greater than 99% reflection at $3.01 \mu\text{m}$, 0° incidence; greater than 90% transmission at $3.15 \mu\text{m}$, 0° incidence; greater than 90% transmission at $3.45 \mu\text{m}$, 0° incidence.
- 30 - **Output coupler 18, first side 34:** 98-99% reflection at $1.61 \mu\text{m}$, 0° incidence; 50% reflection at $3.01 \mu\text{m}$, 0° incidence; greater than 90% transmission at $3.15 \mu\text{m}$, 0° incidence; greater than 90% transmission at $3.45 \mu\text{m}$, 0° incidence.

- **Output coupler 18, second side 36:** greater than 99% reflection at 1.064 μm , 0° incidence; greater than 97% transmission at 3.01 μm , 0° incidence; greater than 90% transmission at 3.15 μm , 0° incidence; greater than 90% transmission at 3.45 μm , 0° incidence.

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The 1.064 μm high reflector coating on the second side 36 of the output coupler 18 allows double pass pumping of the primary process while relieving the first side 30 of the rear reflector 16 from a second high reflective coating band.

10 The above mirror specifications are for a preferred embodiment of the present invention. The specifications need not be exactly those listed. The general strategy is to minimize reflectivity at 3.15 μm and 3.45 μm , while fully containing the 1.61 μm wave, and allowing partial reflectivity for the 3.01 μm wave.

15 In the preferred embodiment, the reflector 16 and coupler 18 are optical thin films disposed on a substrate to provide a mirrored surface. Those skilled in the art will appreciate that any suitable thin film design may be used for this purpose.

20 The described RTA OPO 14 can be used to produce a secondary signal output at 3.01 μm with greater than 25% overall 1 μm to 3.01 μm conversion efficiency. The 3.01 μm output can then be used to pump a second OPO 22 to produce tunable 8-12 μm output as shown in Fig. 1. The efficient conversion of the 1 μm output to 3.01 μm by use of the secondary signal wave in RTA allows the overall 1 μm to 8-12 μm process to proceed efficiently.

25 In the illustrative embodiment, the second OPO 22 uses a silver gallium selenide (AgGaSe_2) crystal 24. Those skilled in the art will appreciate that any suitable crystal may be used for this purpose. For example, a CGA crystal can also be used to generate efficient 8-12 μm tunable radiation when pumped by an efficient 3.01 μm source.

The characteristics of a Type II AgGaSe_2 OPO 22 pumped at 3.01 μm were derived through computer simulation and are summarized below in Table 1.

signal λ (μm)	idler λ (μm)	idler/pump walk-off (mrad)	theta (degrees)	deff (pm/V)	gain coefficient (/sqrt Watt)	crystal angular tolerance (mrad-cm)	OPO acceptance angle (mrad-cm)	OPO acceptance BW (cm ⁻¹ -cm)
4.8	8.0	11.90/11.36	55.5	3.20E+01	2.11E-04	16.70	26.05	15.49
4.5	9.0	12.28/11.66	53.3	3.28E+01	2.11E-04	15.21	28.42	14.06
4.3	10.0	12.48/11.79	52.2	3.32E+01	2.08E-04	14.29	31.12	13.16
4.1	11.0	12.58/11.85	51.7	3.34E+01	2.03E-04	13.66	34.04	12.57
4.0	12.0	12.59/11.85	51.7	3.34E+01	1.98E-04	13.21	37.19	12.17

Table 1

With an internal angular range of 3.8 degrees, the idler wave output from the AgGaSe₂ OPO 22 can cover the full 8-12 μm region. Walk-off losses can be minimized by using the shortest AgGaSe₂ crystal possible in the OPO with the largest possible pump beam waist consistent with OPO threshold considerations. In addition, the signal output from the OPO spanning the 4.0-4.8 μm range can be useful for infrared countermeasure applications and/or biological agent detection.

Thus, the present invention has been described herein with reference to a particular embodiment for a particular application. Those having ordinary skill in the art and access to the present teachings will recognize additional modifications, applications and embodiments within the scope thereof. For example, the present teachings are not limited to the use of optical thin film reflective elements. Any surface which serves to eliminate unwanted energy from the medium may be used for this purpose.

It is therefore intended by the appended claims to cover any and all such applications, modifications and embodiments within the scope of the present invention.

Accordingly,

WHAT IS CLAIMED IS: